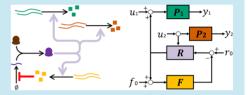
Engineering Translational Resource Allocation Controllers: Mechanistic Models, Design Guidelines, and Potential Biological Implementations

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Supporting Information

ABSTRACT: The use of orthogonal ribosomes in combination with dynamic resource allocation controllers is a promising approach for relieving the negative effects of cellular resource limitations on the modularity of synthetic gene circuits. Here, we develop a detailed mechanistic model of gene expression and resource allocation, which when simplified to a tractable level of complexity, allows the rational design of translational resource allocation controllers. Analysis of this model reveals a fundamental design trade-off: that reducing coupling acts to



decrease gene expression. Through a sensitivity analysis of the experimentally tunable controller parameters, we identify how each controller design parameter affects the overall closed-loop behavior of the system, leading to a detailed set of design guidelines for optimally managing this trade-off. On the basis of our designs, we evaluated a number of alternative potential experimental implementations of the proposed system using commonly available biological components. Finally, we show that the controller is capable of dynamically allocating ribosomes as needed to restore modularity in a number of more complex synthetic circuits, such as the repressilator, and activation cascades composed of multiple interacting modules.

KEYWORDS: resource competition, orthogonal ribosomes, feedback control, modularity

Ensuring circuit modularity, *i.e.*, the independent and predictable functioning of different circuit processes, remains a key goal in synthetic biology. If modules are independent then they can be recombined to produce novel functions that can be predicted from previous characterization. This approach is commonly used in electronics and computer science where complex functions are broken down into independent modules, which can be assembled to form new systems.

However, in synthetic circuits, there is often a failure of modularity, with gene circuits based on purportedly well characterized components needing iterative rounds of redesign and re-experimentation to obtain functional implementations. Modularity fails for a variety of reasons: (i) unexpected cross talk between modules due to component reuse, (ii) subtle changes in gene regulation due to unforeseen effects of combining DNA sequences, (iii) retroactivity effects where the titration of a transcription factor to a downstream module affects the behavior of the upstream module,³ and, (iv) the use of a common limited pool of resources for gene expression.⁴ Careful selection of components can ameliorate the effects of (i) by ensuring modules do not have off target effects. The introduction of "insulator elements" such as ribozymes can reduce the effects of (ii)⁶ and the development of buffer circuits allows loading fracture due to retroactivity (iii) to be reduced. The question of how to optimally manage the effects of cellular resource limitations on circuit modularity, however, remains an open problem.

During exponential growth, the concentration of RNA polymerases (RNAP) and ribosomes in the cell remains constant. This results in a fixed pool of gene expression resources. While both resources are finite, numerous experimental studies have shown it is the number of free ribosomes in system that is the main limitation on gene expression. The sharing of this fixed resource across genes leads to a phenomenon known as gene-coupling. This results in the emergence of nonregulatory interactions between coexpressed genes, since each synthetic circuit module will utilize as many ribosomes as possible at any one moment, as determined by parameters such as mRNA levels or RBS strength.

To illustrate the problem mathematically, consider the number of free ribosomes as a function of the ribosome supply and demand as

$$R(\phi_1) = \frac{R_{\text{total}}}{1 + \phi_1} \tag{1}$$

where R_{total} is the total number of ribosomes available and ϕ is the demand.^{4,10} Upon the addition of another demand ϕ_2 , the free ribosome number becomes

$$R(\phi_1, \, \phi_2) = \frac{R_{\text{total}}}{1 + \phi_1 + \phi_2} \tag{2}$$

Received: January 18, 2018 Published: October 15, 2018



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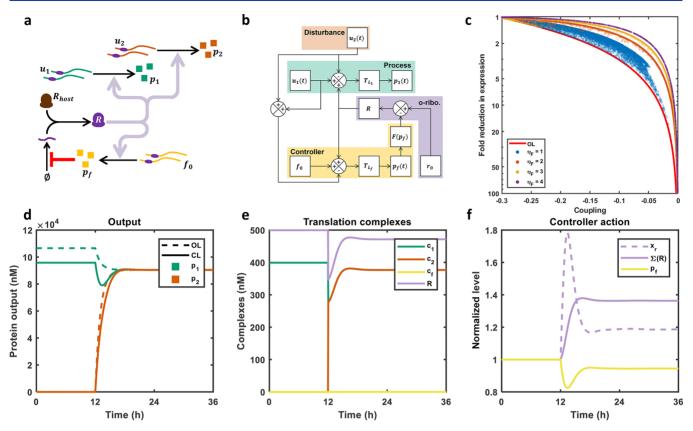


Figure 1. Development of a genetic feedback controller model. (a) Schematic of the negative feedback loop implementation. (b) Block diagram of the controller. The process, highlighted in green, converts the input u_1 into protein output p_1 utilizing the o-ribosome pool R. The input into a second process (not shown) u_2 acts as a disturbance to the first process which is ameliorated by the effect of the controller. The controller protein is constitutively expressed (f_0 signal) so the output p_f is dependent upon R. As inputs u_i disturb R the level of p_f changes (i.e., as u_i increases, p_f decreases). As p_f is a repressor the disturbance signal is inverted in the $F(p_f)$ block. (c) Gene expression and decoupling trade-off. Expression and coupling were calculated as defined in the Methods. The results of the multiobjective optimization where perturbed by ±50% to discover the shape of the true Pareto front. The controller results are divided by $η_f$, N = 107.743. OL, open loop trade-off determined by varying the values of the inputs for a circuit using the host ribosome pool, which by definition is uncontrolled. (d-f) Controller dynamics as it decouples circuit genes using the parameters of Point 19 of Table S1. The first gene p_1 is constitutively expressed throughout, $u_1 = 500$ nM throughout. At 12 h, u_2 rises from 0 to 500 nM. (d) Protein output of the close loop system. OL represents the coupling when the inputs are tuned in the absence of the controller to match the final protein level. (e) Translation complexes: Changing distributions of orthogonal ribosomes across circuit and controller mRNAs. c_1 , c_2 and c_f represent the translation complexes of the mRNAs of genes 1, 2 and the regulator f respectively. R represents the free orthogonal ribosomes. c_f acts as the sensor for the disturbance at t = 12 h. Levels are normalized by value at t = 12. u_1 controller action: Changes in controller components over time. Levels are normalized by value at

As $\phi > 0$ in all cases, by definition $R(\phi_1, \phi_2) < R(\phi_1)$. This decrease in free ribosome number reduces the rate of downstream processes, such as mRNA-ribosome binding, as a consequence of the law of mass action. This leads to a decrease in other modules as a new module is induced (this is often termed coupling^{4,13,15}): activation of one circuit module effectively inhibits other modules. In this case the supply of ribosomes (the numerator) is determined by the cell and supply is constant regardless of the demand (the denominator)—*i.e.*, there is no control of R_{total} .

To mitigate this decrease in free ribosomes upon the addition of new genes, consider a system where the supply of total ribosomes can be matched to the circuit's demand for ribosomes. Let this malleable ribosome pool be R':

$$R(\phi_1) = \frac{R'_{\phi_1}}{1 + \phi_1} \tag{3}$$

Upon the addition of another gene the demand (the denominator) increases as before:

$$R(\phi_1, \phi_2) = \frac{R'_{\phi_1, \phi_2}}{1 + \phi_1 + \phi_2} \tag{4}$$

However, in this ideal system we can now increase the supply of R' (*i.e.*, increase the numerator) to make $R(\phi_1) = R(\phi_1, \phi_2)$. This maintains the free ribosome pool available to the circuit and so removes ribosome-mediated gene coupling.

In a previous work, we have experimentally realized a prototype of a feedback controller that can dynamically allocate more ribosomes to the circuit when required. Increasing total ribosome number is not biologically feasible, so our controller acts to dynamically allocate the translational capacity *between* host and circuit genes in response to circuit demand, thus relieving the effects of resource limitations on the circuit. This is achieved by regulating the production of a pool of quasi-orthogonal ribosomes. These specialized circuit-specific ribosomes can be created by expressing an orthogonal 16S rRNA and replacement of the natural ribosome binding site in circuit genes, or other genes of interest, with complementary synthetic

ribosome binding sites. The o-16S rRNA replaces the endogenous host 16S rRNA in a fraction of the host ribosomes creating a separate translational resource that is targeted to circuit genes by binding the complementary synthetic RBS sequence. By placing the production of the o-16S rRNA under the control of a constitutively expressed repressive transcription factor, which itself uses the orthogonal ribosome pool for its own translation, we created a feedback controller that produces o-16S rRNA, and hence orthogonal ribosomes, in response to circuit demand. As circuit genes are induced, they sequester oribosomes for their own expression resulting in a fall in the expression of the regulator. This relieves the repression of the o-16S rRNA, resulting in increased o-16S rRNA production and increased o-ribosome co-option. Thus, the controller implements a negative feedback loop. See Figure 1a for a schematic of the biological implementation of this feedback loop. Of course, the controller cannot mitigate intrinsic limitations arising from the fact that the total number of ribosomes in the cell is finite. Rather, the controller acts to dynamically manage the allocation of translational activity between host and circuit genes in the most efficient way, by increasing circuit capacity as circuit demand requires it.

In this paper, we use the biological insights gained from the prototype to produce simple models of the controller architecture that can be used to inform detailed design of the systems dynamics using control theory metrics. Using such models, we demonstrate how improved resource allocation controllers can be rationally designed to decouple the expression of different genes, and develop design rules for how the tuning of different controller design parameters can act to separately specify either the dynamic response time or overall protein output (*i.e.*, gain) of the circuit. On the basis of these design rules, we identify and evaluate a number of alternative potential experimental implementations of the proposed translational controllers. Finally, we demonstrate the potential of resource allocation controllers to improve the modularity of a variety of complex gene circuits.

RESULTS AND DISCUSSION

Mechanistic Model of the Resource Allocation Controller. We initially develop a complete mechanistic model of gene expression and the action of the controller, before investigating how this model can be simplified for use as a design tool. We assume that each circuit promoter (g_i) can be bound by a multimeric transcription factor (u_i) to form a promoter complex (κ_i) capable of recruiting a free RNA polymerase (σ) to form a translation complex. When transcription occurs, an mRNA (m_i) is produced, and the original RNAP polymerase and promoter complex are released. The above interactions are described by the following chemical reactions:

$$g_i + \eta_i \cdot u_i \overset{\alpha_{f_i}}{\underset{\alpha_{r_i}}{\rightleftharpoons}} \kappa_i \quad \kappa_i + \sigma \overset{\xi_{f_i}}{\underset{\xi_{r_i}}{\rightleftharpoons}} x_i \quad x_i \overset{\tau_i}{\rightarrow} m_i + \sigma + \kappa_i$$

The mRNA is bound by a free orthogonal ribosome, R, to form a translation complex (c_i) . Upon translation, a protein (p_i) is produced and the mRNA and R are released:

$$m_i + R \stackrel{\beta_{f_i}}{\rightleftharpoons} c_i \quad c_i \stackrel{\gamma_i}{\rightarrow} m_i + R + p_i$$

Additionally, both mRNAs and proteins degrade at rates δ_{m_i} and δ_{v_i} respectively.

Applying the law of mass action we derive the following ODEs describing the time evolution of the circuit components:

$$\dot{\kappa}_i = \alpha_f g_i u_i^{\eta_i} - \alpha_{r_i} \kappa_i - \xi_{f_i} \kappa_i \sigma + \xi_{r_i} x_i + \tau_i x_i \tag{5}$$

$$\dot{x}_i = \xi_{f_i} \kappa_i \sigma - \xi_{r_i} x_i - \tau_i x_i \tag{6}$$

$$\dot{m}_i = \tau_i x_i - \beta_{f_i} m_i R + \beta_{r_i} c_i + \gamma_i c_i - \delta_{m_i} m_i$$
(7)

$$\dot{c}_i = \beta_{f_i} m_i R - \beta_{r_i} c_i - \gamma_i c_i \tag{8}$$

$$\dot{p}_i = \gamma_i c_i - \delta_{pp} p_i \tag{9}$$

This represents a simple single-input-single-output (SISO) motif and forms the basis of our model. Complex circuits can be constructed by letting the output from one module form the input to another.

To implement our controller we first consider the conversion of host ribosomes $(R_{\rm H})$ into circuit-specific orthogonal ribosomes (R). The orthogonal 16S rRNA gene promoter (g_r) recruits σ to form a translation complex (x_r) which produces the orthogonal rRNA (r):

$$g_r + \sigma \overset{\xi_{f_r}}{\underset{\xi_{r_r}}{\rightleftharpoons}} x_r \quad x_r \overset{\tau_r}{\rightarrow} r + \sigma + g_r$$

The orthogonal 16S rRNA binds host ribosomes, R_H , and so recruits ribosomes to the circuit-only orthogonal pool, R:

$$R_{\rm H} + r \stackrel{Q_r}{\rightleftharpoons} R$$

In the presence of the controller the orthogonal rRNA gene is regulated by the repressor p_f . The repressor binds the free g_r promoter and prevents the binding of RNA polymerase and associated factors (σ in our model):

$$g_r + \eta_f \cdot p_f \stackrel{\alpha_{r_r}}{\underset{\alpha_{f_f}}{\rightleftharpoons}} \kappa_f$$

We model expression of the regulator protein by considering the constitutive expression of its mRNA from an unregulated promoter, g_i :

$$g_f + \sigma \stackrel{\xi_{r_f}}{\rightleftharpoons} x_f$$

We model the transcription and translation of the repressor's mRNA and protein in the same manner as the circuit genes, as described above. Applying the law of mass action results in the following ODEs describing the production of the repressor and intermediate complexes:

$$\dot{g}_f = -\xi_f g_f \sigma + \xi_{r_f} x_f + \tau_f x_f \tag{10}$$

$$\dot{x}_f = \xi_{f_f} \kappa_f \sigma - \xi_{r_f} x_f - \tau_f x_f \tag{11}$$

$$\dot{m}_f = \tau_f x_f - \beta_{f_f} m_f R + \beta_{r_f} c_f + \gamma_f c_f - \delta_{m_f} m_f$$
(12)

$$\dot{c}_f = \beta_{f_f} m_f R - \beta_{r_f} c_f - \gamma_f c_f \tag{13}$$

$$\dot{p}_{f} = \gamma_{f}c_{f} - \delta_{p_{f}}p_{f} - \eta_{f}\alpha_{f}g_{r}p_{f}^{\eta_{f}} + \eta_{f}\alpha_{r}\kappa_{r} \tag{14}$$

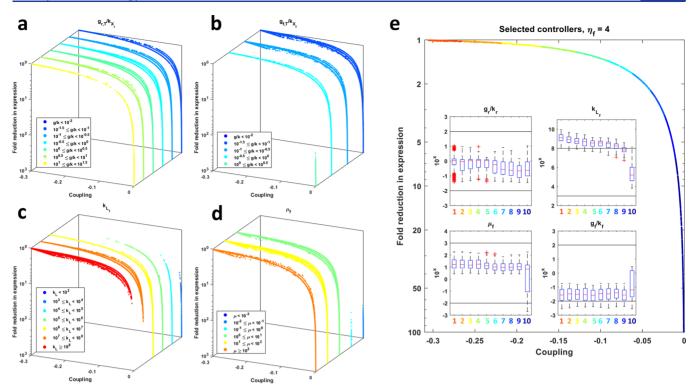


Figure 2. Design trade-offs between gene expression and decoupling. Designs of controllers that manage the trade-off between gene expression and decoupling. Expression and coupling are calculated as defined in the Methods. $N = 107\,743$. As described in the main text, controllers where $\eta_f = 1$ are removed from the following panels for clarity. Also note that the third axis in plots (a–d) and subsequent separation serves only to aid visualization and does not represent parameter value, which is indicated by the color as outlined in the figure legend. Points with greater fold reduction than 10^3 are not shown. All these points represent complete decoupling. (a) o-rRNA transcription as determined by the $g_{f,T}/k_{X_f}$ ratio. (b) Transcription of the controller protein as determined by the $g_{f,T}/k_{X_f}$ ratio. (c) Controller mRNA ribosome binding site strength as measure by mRNA-ribosome dissociation constant k_{L_f} (d) Controller protein g_r dissociation constant μ_{f^*} (e) Parameter changes across the Pareto front (i.e., controllers where $\eta_f = 4$). The different trade-offs between coupling and expression are divided into similarly behaving controllers (as described in the Methods). Insets show the median parameter value and interquartile range for each set of behaviors.

Applying the law of mass action to the o-rRNA promoters and ribosome species yields

$$\dot{g}_r = -\xi_{f_i} g_r \sigma + \xi_{r_i} x_r + \tau_r x_r - \alpha_{f_i} g_r p_f^{\eta_f} + \alpha_{r_i} \kappa_r \tag{15}$$

$$\dot{x}_r = \xi_{f_r} g_r \sigma - \xi_{r_r} x_r - \tau_r x_r \tag{16}$$

$$\dot{\kappa}_r = \alpha_f g_r p_f^{\eta_f} + \alpha_r \kappa_r \tag{17}$$

$$\dot{r} = \tau_r x_r - \delta_r r - \varrho_f r R_H + \varrho_r R \tag{18}$$

$$\dot{R}_{\rm H} = -\varrho_{\rm f} r R_{\rm H} + \varrho_{\rm r} R \tag{19}$$

This detailed model is highly complex, being composed of 5 species per circuit gene and the 10 species of the controller. Additionally, some parameters, such as on and off rates, are difficult to determine experimentally and so they are unlikely to be available in the literature preventing design. We reduce this model by considering the effect of time-scale separation and species conservation (see Section S1). Additionally, we remove the potentially confounding RNA polymerase mediated coupling as discussed in Section S1. The tractable model is composed of 3 ODEs describing the action of the controller and one equation per circuit protein:

$$\dot{p}_{i} = \gamma_{i}\hat{c}_{i}R - \delta_{p_{i}}p_{i} \tag{20}$$

$$\dot{p}_{f} = \gamma_{f} \hat{c}_{f} R - \delta_{p_{f}} - \eta_{f} \overline{g}_{r} p_{f}^{\eta_{f}} + \eta_{f} \mu_{f} \overline{\kappa}_{r}$$
(21)

$$\dot{r} = \tau_r \overline{x}_r - \delta_r r - \varrho_f r R_H + \varrho_r R \tag{22}$$

$$\dot{R}_{\rm H} = -\varrho_{\rm f} r R_{\rm H} + \varrho_{\rm r} R \tag{23}$$

where \hat{c} is a measure of the demand for ribosomes and includes the quasi-steady state transcriptional dynamics. \hat{c} is defined fully in eq S10. \overline{g}_r and $\overline{\kappa}_r$ are the quasi-steady state free and inhibited orRNA promoter concentrations respectively (eqs S12 and S14). The concentration of free orthogonal ribosomes is given by

$$R = \frac{R_{\text{total}} - R_{\text{H}}}{1 + \hat{c}_f + \Sigma_1^N(\hat{c}_i)}$$
(24)

Note that this follows the same form as eq 2, with the total number of o-ribosomes available to the circuit being the total number of all ribosomes ($R_{\rm total}$) minus the number of host ribosomes ($R_{\rm H}$). (Note that the majority of this work is concerned with two gene circuits and therefore N=2.)

Model Analysis Reveals a Trade off between Gene Expression and Level of Decoupling. We considered a simple circuit consisting of two modules single-input-single-output motifs. We assess the impact of the controller to reject disturbances to one module upon activation of the second: *i.e.*, we assess the change in p_1 upon activation of u_2 . This difference in expression of p_1 due to the u_2 disturbance is termed "coupling"

below (see Methods for quantification). We assess any impact on protein levels by comparing the final protein outputs to the theoretical maximum: i.e., the protein levels obtained using the host ribosome pool for translation and assuming maximal induction. We initially consider how tuning the circuit inputs (u_1 and u_2) only impacts gene expression and coupling in a circuit translated by the host ribosome pool (and therefore in the absence of feedback control). This demonstrates a linear tradeoff with coupling falling as expression falls. Using the reduced five state model to design our feedback controller, we carried out a multiobjective optimization of the experimentally tunable controller parameters aiming to produce both high protein levels and low gene coupling (see Methods). We sampled parameters around the front to identify the true shape of the Pareto-optimal front, corresponding to a controller cooperativity η_f of 4. This identified a hard trade-off between these two objectives, with the range of equally optimal solutions showing an inverted concave shape, i.e., decreases in gene coupling are achieved at the expense of decreases in gene expression (Figure 1c). Our simulations suggest that the controller can halve coupling for only a 13% reduction in expression (for the highest cooperativity $\eta_f = 4$); in comparison the tuning circuit inputs requires a 48% reduction in expression to achieve the same level of coupling. If a loss of ~50% is acceptable then coupling can be reduced to only 5%. The controllers give access to a higher level of gene expression for a given level of decoupling than tuning circuit parameters alone.

We demonstrate the functioning of the controller using Point 9 as determined by our optimization routine. This controller design shows intermediate results with coupling falling to only 5% for a loss of 50% expression. The corresponding open loop arrangement where the inputs u_1 and u_2 tuned to produce the same final expression shows coupling of 15%. The controller successfully insulates one gene from the induction of another (Figure 1d), bar a short transient disturbance (<12 h). Tracking the concentrations of the intermediate species reveals the operation of the controller; with translation of p_f falling and the number of o-rRNA genes being transcribed increasing as the second gene is induced (Figure 1e). This results in a net increase in the number of orthogonal ribosomes (Figure 1f), which means that in the long term the translation complexes producing each protein do not change (Figure 1d).

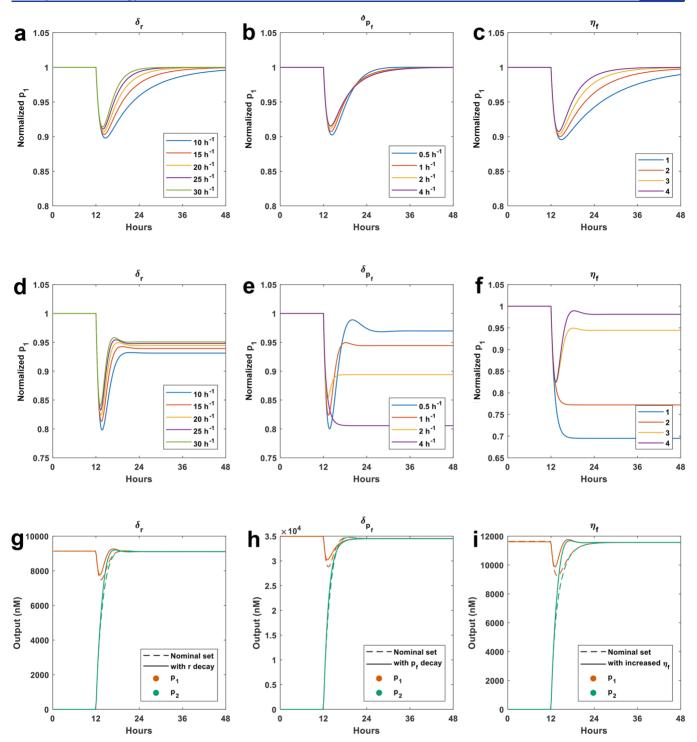
To identify the true Pareto front and determine the robustness of the trade-off we varied the results of our genetic algorithm by up to 50% for each point identified. This identifies the true Pareto front when $\eta_f = 4$. None of the designs from this robustness analysis falls below the linear trade-off achieved by input tuning; i.e., there are no designs where the action of the controller reduces expression without having a beneficial effect on gene coupling. A number of controllers provide no improvement upon input tuning (see below). We find that a small number of these perturbed designs show slower responses, and we discount these from further analysis. We carried out an additional robustness analysis allowing all parameters governing the controller behavior to vary. This includes parameters that are either difficult to design (e.g., controller translation rate γ_f) or intrinsic properties which cannot be designed (e.g., o-rRNA association rate, μ_r). All of these controllers also fall upon the same front demonstrating that uncertainty in these values does not preclude controller design (Figure S1).

To determine how each parameter contributes to the gene expression and coupling trade off, we analyzed how each changes across the front. This highlights the need for high η_f values. This

parameter represents the level of cooperativity in the system brought about, for example, by transcription factor multimerization or the presences of multiple operator sites. The true Pareto front coincides with a value of $\eta_f = 4$ (Figure 2b). Due to the present constraint that most repressors used in synthetic biology are derived from natural sources, it is therefore unlikely that all combinations of multimerization (η_f) , dissociation constant (μ_f) and promoter kinetics (k_X) desired will be present in one selected repressor, and so we also consider designs based on suboptimal dimeric and trimeric repressors ($\eta_f = 2$ and 3). However, given the poor performance of monomeric controllers $(\eta_f = 1)$, we discount these from all further analysis. Across all η_f values, small μ_f values are most often associated with controllers which act to nearly completely decouple genes but at a significant cost to gene expression (Figure 2d) with only μ_f > 1 nM giving access to moderately high levels of expression. Similarly, small k_{L_i} values, corresponding to strong ribosomes binding sites (low ribosome-mRNA dissociation constant), are associated with large levels of decoupling at a high cost to gene expression (Figure 2c). Simulations suggest $k_{L_f} > 10^5$ nM and μ_f > 0.1 nM in all cases, for the simple two gene circuit example used here. (Note that for many natural transcription factors coopted into synthetic gene networks $\mu_f < 0.1$ nM and η_f may be limited. We demonstrate how this can be compensated for in controller design in the section Dynamic Resource Allocation Controller Restores Modularity in a Range of More Complex Gene Circuits below). A high $g_{f,T}/k_{X_f}$ ratio $(g_{f,T}/k_{X_f} > 1$, produced by expressing the regulator from a strong promoter carried on a high copy number plasmid) results in complete decoupling and abolition of gene expression (Figure 2b). We therefore suggest keeping $g_{f,T}/k_{X_f}$ < 1 in all instances. We find that the $g_{r,T}/k_{X_r}$ ratio governing maximal o-rRNA transcription rate varies significantly across all behaviors, making general guidelines difficult to establish (Figure 2a).

To provide further specific quantitative design rules that manage the trade-off, we divided the responses of the different controllers based on the their decoupling ability and final circuit expression level (Figure 2e). These represent groups of controllers with similar behaviors, see Methods. This shows that the key determinant of the expression-coupling trade-off is the RBS strength (k_L) with the dissociation constant decreasing with increased decoupling (Figure 2e, inset). (Note that for the majority of behaviors k_{L_t} is greater than 10^8 nM. This represents a weaker RBS strength than currently available requiring extensive RBS engineering.) The o-rRNA transcriptional parameters $(g_{r,T}/k_{X_r} \text{ ratio})$ is between 0.1 and 1, which can be achieved through a range of different plasmid copy number and promoter dissociation constants (Figure 2e, inset. Figure S4). The gene encoding the controller protein should be expressed from a weak promoter and a low or medium copy plasmid in order to create a $g_{f,T}/k_{X_f}$ ratio of between 0.01 and 0.1 (Figure 2e, inset). The controller dissociation constant μ_f can take any value between 10 nM and ~30 nM. For the most strongly decoupling controllers a greater range of $g_{f,T}/k_{X_f}$ and μ_f are tolerated, with the greater range corresponding to a higher expression of controller and stronger repressor binding. The same patterns are observed across $\eta_f = 2$ and 3 (Figure S2).

Designing System Response Times by Tuning Controller Parameters. Analysis of the controllers tested so far has focused on how they are able to correct steady state errors



brought about by gene coupling and so we have largely ignored the system dynamics, bar excluding excessively slow controllers (*e.g.*, penalizing simulations which only reach steady state after >24 h). However, a controller that decouples genes well but has a slow response time will not be suitable for many applications in

synthetic biology. Therefore, we took the previous candidate controllers and conducted a local sensitivity analysis around each design point to assess the impact of each parameter on the system's speed of response. In addition to the controller parameters varied so far we also varied δ_{ρ} , δ_{m_t} and $\delta_{p\theta}$ which

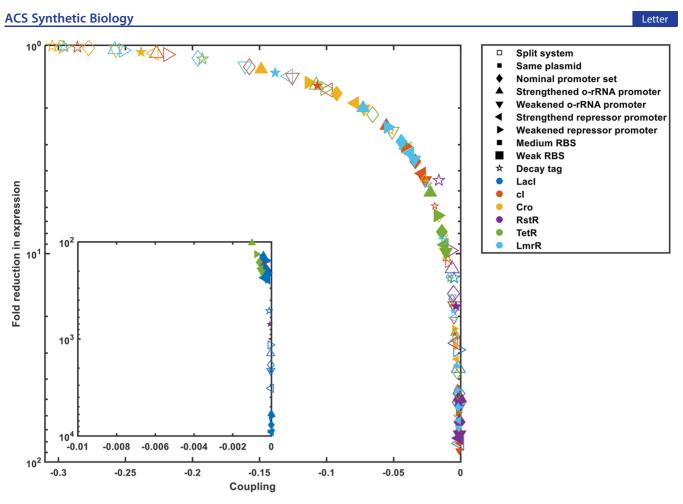


Figure 4. Comparison of biological implementations based on orthogonal repressors. Simulations of implementations based on the repressors in different plasmid confirmations and with degradation motifs. (a) The positions of the prototype controllers in the coupling-expression space. Inset, expansion of the main figure around point (0, 100). Point colors represent the regulator protein and point style denotes copy number as follows: Same plasmid, $g_{r,T} = g_{f,T} = 100$ nM; Chromosomal, $g_{r,T} = 500$ nM and $g_{f,T} = 10$ nM. Decay tag, $g_{r,T} = 500$ nM, $g_{f,T} = 10$ nM, $\delta_{v_r} = 3$ h⁻¹ $\approx t_{1/2} = 8$ min, equivalent to LVA tag.²²

represent the decay of the o-rRNA, controller mRNA and controller protein, respectively. These parameters were kept constant in the previous design evaluations to minimize the number of parameters in the optimization, but since decay parameters often have significant affects on speed of response we explicitly assess their impact here.

The o-rRNA decay constant (δ_r) and protein controller decay constant (δ_{p_i}) are key to determining the speed of the system response. Increasing both parameters acts to increase the speed of response (Figure 3). Increasing δ_r increases the controllers ability to decouple circuit genes. Increasing δ_{p_f} decreases decoupling ability but increases expression. In the regions tested, varying δ_r is less likely to introduce significant overshoots into the system (as seen at low δ_{p_i} values). However, a greater range of speed-up is achievable by varying the protein decay constant. The latter is also a more experimentally tractable parameter. Increasing both parameters acts antagonistically, with increases in δ_r decreasing gene coupling and increases in δ_v increasing it, meaning tuning both parameters may be advantageous. We see very little impact from varying the mRNA decay rate (δ_m). As previously discussed the value of the controller cooperativity (η_f) is a key determinant of controller decoupling ability. This analysis replicates this result and also highlights that, at least in this parameter regime, increasing cooperativity also acts to significantly increase the speed of response (Figure 3).

Given that changing these three parameters significantly changes the decoupling ability of the controller in addition to its dynamics, we assessed the impact of varying additional parameters to design controllers with increased response times while maintaining controller function (as measured by decoupling and expression). The changes in decoupling ability brought about by increasing δ_r can be ameliorated by decreasing the expression of the controller protein through tuning g_{tT}/k_{χ_t} (Figure 3g). While in Figure 3g, the time it takes for p_1 to return to steady state after induction of p_2 at 12 h does not change the p_2 rise time (i.e., the time it takes for p_2 to rise from 10% to 90% of its final value) falls by 30%. The loss in decoupling ability associated with increasing the controller protein decay rate can likewise be corrected by increasing $g_{f,T}/k_{X_f}$ (Figure 3h). In Figure 3i, the dynamics are significantly improved by increasing η_f from 2 to 4 with the p_1 settling time falling by 5 h. To maintain expression levels μ_f of the controller protein needs to be tuned, but this may not be possible given the reuse of natural components as discussed above.

Potential Biological Implementations of the Controller Designs. We carried out a detailed literature review to identify potentially suitable repressors with which to implement our system, focusing our analysis on (i) the ability of the

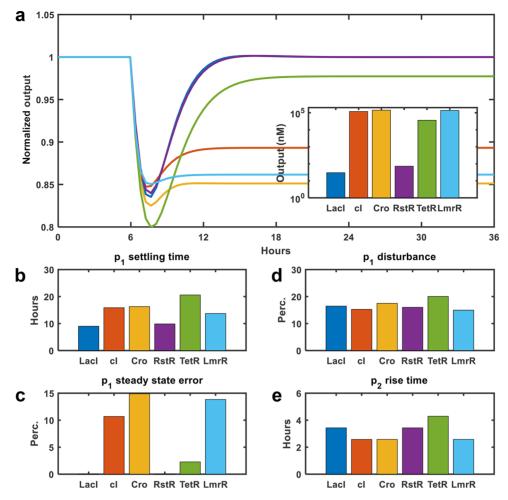


Figure 5. Dynamic responses of potential biological implementations. Characterization of the response of p_1 to the disturbance caused by u_2 . Designs are available in Table S5. (a) Circuit dynamics showing the normalized levels of protein 1. Inset, steady state output at t = 48 h. (b) p_1 settling time. The number of hours from the induction until p_1 returns to steady state. (c) p_1 steady state error. The difference between p_1 (t = 48) and p_1 (t = 12). (d) p_1 disturbance. The percentage fall in p_1 upon u_2 induction. (e) p_2 rise time. The time it takes for p_2 to increase from 10% of its steady state to 90% of its steady state.

repressor to be expressed in bacterial hosts (*i.e.*, repressors from bacteria or bacteriophage), (ii) orthogonality (*i.e.*, repressors that are not used in fundamental host processes), (iii) the presence of a known promoter architecture (which could be used to infer the dissociation constant of the RNA polymerase, see Section S2) and (iv) detailed characterization of binding kinetics (ideally dissociation constants measured in a biochemical assay, rather than a constant inferred from device function such as by fitting a Hill function to induction—fluorescence curves, as is often the case). We identified six repressors from this literature search, including the commonly used LacI, TetR¹⁷ and cI¹⁸ repressors. We also identified putative controller candidates Cro and RstR from bacteriophages PY54, CTX φ^{20} and LmrR, a global regulator of antibiotic resistance from Gram positive *Lactococcus lactis*.

Using the results of our sensitivity analysis and additional biological constraints we identified a number of feasible biological implementations. We considered two gene expression systems: (i) where the o-rRNA and regulator having the same medium copy number (mimicking placement in the same plasmid, such as ColE1) and (ii) a high copy number o-rRNA gene, carried on for example a pUC vector, and a chromosomally integrated regulator. Note that we did not assess the potential designs requiring the o-rRNA and regulator to be carried on

different copy number plasmids, as these would result in high burden on the cells and significantly decreased growth rate as these cells would need to carry at least three plasmids, one containing circuit genes and one each for the o-rRNA gene and regulator. We explored the potential impact of engineering the o-rRNA promoter strength by multiplying the reported dissociation constant (as reported in the literature or calculated see Section S2) by 0.25 (representing a 4-fold strengthening of the promoter) and 2 (representing a 2-fold weakening of the promoter). We simulated three different controller promoter strengths representing strong (200 nM), medium (500 nM) and weak (1000 nM) promoters. We also assessed the impact of varying RBS strength. We also assessed the impact of fusing degradation tags to the controller protein. The small amino acid motifs acts to target proteins for degradation and hence increase δ_{ν} , These simulations of potential controller designs shows that by selecting different biological components all levels of the trade-off are accessible. (Figure 4).

These different implementations have a wide range of dynamics. Selecting those controllers with high decoupling ability (*i.e.*, where coupling was greater than -0.15), we ranked them by the length of time it took p_1 to return to steady state after the disturbance caused by u_2 and selected the fastest responding implementation for each repressor (Figure 5). See

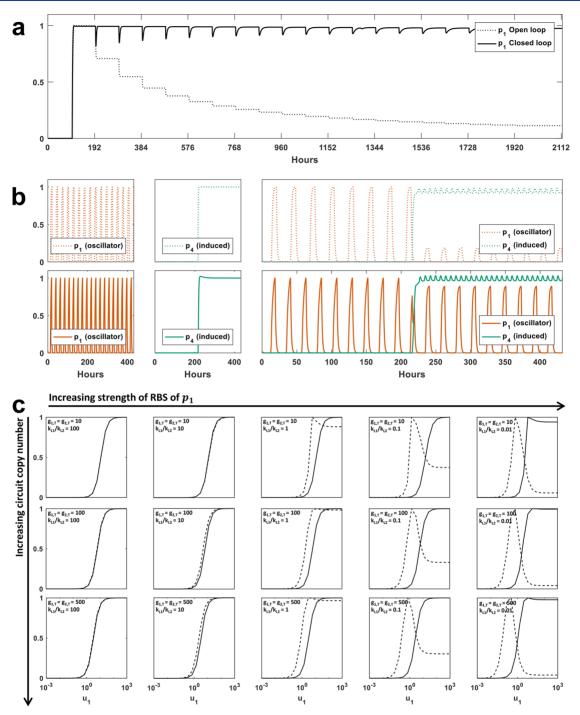


Figure 6. The controller rescues modularity in a variety of circuit contexts A range of common circuits were simulated in both the open and closed loop confirmations. All y-axes are normalized output. (a) The controller successfully renders a gene invulnerable to the induction of many additional genes at 100 h intervals. Other genes not shown. (b) Maintaining repressilator behavior in the presents of an induced gene. The repressilator (protein p_1 to p_3 , only p_1 is shown) is simulated before an additional gene p_4 with a stronger RBS is induced. Upper panels: Open loop (no controller). Lower panels: Closed loop (with controller). Left and center panels: Function of the individual modules alone. Right: Function of the two modules in one circuit. p_4 is induced at 24 h. (c) The controller removes resource limitation-induced failure in the design of an activation cascade $(u_1 \rightarrow p_1 \rightarrow p_2)$. In the absence of the controller (dashed line) some prototype designs do not show the monotonically increasing output of p_2 to u_1 as desired in an activation cascade. The controller removes these resource limitations allowing the circuit to function as expected across all prototype designs.

I

Table S5 for details of the designs shown. All these implementations have similar p_2 rise times of approximately 3 h and show similar disturbances to p_1 upon induction of u_2 (Figure 5, e). The putative controllers based on the tetramers LacI and RstR show the fastest respond times with p_1 settling with 10 h of p_2 induction (Figure 5b). The designs based on

dimers show the greater outputs, with a concurrent increase in coupling between 7 and 14% depending upon the controller design (Figure 5c).

Dynamic Resource Allocation Controller Restores Modularity in a Range of More Complex Gene Circuits. Having successfully demonstrated the ability of the proposed

approach to decouple two independent modules, we analyze the ability of the controller to remove resource dependent failure in a variety of more complex gene circuits (Figure 6).

We initially simulate multiple SISO modules with new modules being activated at different intervals. In the absence of the controller, activation of each additional module has an impact on the previously activated modules. For example, the expression of the first module p_1 falls by over 50% as three additional genes are induced. As shown in Figure 6a, the controller successfully eliminates this coupling, making p_1 relatively insensitive to the induction of over 10 additional genes (although note that the rise time and settling time increase slightly with the induction of each additional gene).

A key aim of synthetic biology is that previously characterized components or devices can be introduced into the same cell to form a complex circuit. Here we assess the effect of introducing two separately characterized devices into one complex circuit; i.e., we want to investigate what is the effect of introducing an additional resource consumer on a previously characterized device. As the production of robust genetic oscillators to create clocks for temporal processes functions is of fundamental importance in synthetic circuit design, we consider designs for the repressilator clock and an additional SISO module. These modules are first simulated separately, as shown in (Figure 6b, upper panel). Upon linking these separate devices through a common pool of resources, i.e., coupled through their competition for ribosomes, we see that p_4 induction destroys the oscillations of the repressilator (Figure 6b, upper right panel). If, however, we consider the design of these two devices in the presence of the controller and then introduce them into the same resource pool as before, we see that circuit function is now maintained (Figure 6b, lower panels). Note that while there is still a small loss in repressilator amplitude upon induction of p_4 this is significantly reduced, thus staying closer to the original device behavior.

It has previously been shown that resource limitations can change the input-output response of a simple genetic activation cascade. The authors show that if the upstream module has a stronger ability to sequester ribosomes than the downstream module (a small k_{L_1} -to- k_{L_2} ratio) then the expected response determined from simple Hill-function type modeling (i.e., an increasing output to increasing input in a step-like fashion) can become biphasic or even invert (Figure 6c, dotted open loop lines). We simulate a range of prototype activation cascades in the absence and presence of our controller. In the absence of the controller, no additional resources are available as demand increases, and so we see the activation cascade failing in the same manner as found in Qian et al. In the presence of the controller, the desired behavior of the activation cascade is restored, as translational capacity is directed to the circuit as demand increases. The controller acts to remove the resource limitation, thus allowing simpler models, which often do not account for limited cellular resources, to be used to produce circuit designs that then function as expected in vivo.

CONCLUSIONS

Numerous genetic components and devices have been developed to ensure predictable gene expression or dampen the effect of loading in genetic circuits. However, to date, little attention has been paid to developing genetic devices that are capable of relieving cellular resource limitations. Controllers for orthogonal transcriptional activity based on phage RNA

polymerases have been developed, 23,24 and we have previously implemented a prototype translational controller. 14 Here, we develop a detailed mechanistic model of gene expression and resource allocation, which when simplified to a tractable level of complexity, allows the rational design of optimal translational controllers. We demonstrated that this new model allows the design of controllers that can dynamically allocate orthogonal ribosomes to synthetic circuits within reasonable timeframes (<12 h). Using our model, we identify a fundamental trade-off in controller design: that reducing coupling acts to decrease gene expression. We determined how each controller design parameter affects the overall closed-loop behavior of the system, leading to a detailed set of design guidelines for optimally managing this trade-off. We find that both controller cooperativity and RBS strength are key parameters in determining the level of decoupling that can be achieved. On the basis of our designs, we identified and evaluated a number of alternative potential experimental implementations of the proposed system using commonly available biological components. Finally, we showed that our controller is capable of dynamically allocating ribosomes as needed to restore modularity in a number of more complex synthetic circuits, such as the repressilator, and activation cascades composed of multiple interacting modules.

METHODS

Numerical Simulations. All models were implemented in either MATLAB 2016b and 2017a (The MathWorks Inc., MA, USA) and simulated using the in-built stiff solvers *ode15s* and *ode23s* using increased tolerances (Relative 10^{-6} and Absolute 10^{-6}). Simulations were deemed to have reached steady state when the maximum of the calculated derivative was less than 10^{-2} (relaxed) or 10^{-3} (strict). Additional specialist functions as needed were utilized from the Optimization Toolbox (Version 7.4) and Parallel Computing Toolbox (Version 6.8 or 6.10).

Assessment of Controller Function. The behavior of controllers was characterized by simulating the action of a simple two gene circuit. Initially, the behavior of one gene p_1 is simulated before its response is assessed to the induction of a second gene p_2 at time $t = \theta_{\text{ind}}$. Coupling and expression are normalized:

coupling =
$$(p_1(t = \theta_{ind}) - p_1(t = \theta_{ss}))/p_1(t = \theta_{ind})$$
 (25)

expression =
$$(p_2(t = \theta_{ss}) - p_{target})/p_{target}$$
 (26)

We calculate the fold reduction in expression by taking:

fold reduction in expression =
$$\frac{1}{1 - \text{lexpression}}$$
 (27)

Optimization. The multiobjective optimization was carried out using the inbuilt function gamuliobj with a population size of 200 individuals and with a Pareto fraction of 0.25 from the Optimization Toolbox. k_X values were set to 1 allowing the \hat{x} ratios to be investigated by varying $g_{r,T}$ and $g_{f,T}$ only. See Section S2 for a discussion of permissible parameter bounds. The parameters varied (and their scale and bounds) were $g_{r,T}/k_{X_r}$ ratio (log10 scale, $10^{-2}-10^2$), k_{L_f} (log10 scale, 10^3-10^8), η_f (integers values only to represent the number of required monomers in the DNA binding complex, 1-4), μ_f (log10 scale,

 $10^{-2}-10^3$) and $g_{r,T}/k_{X_r}$ ratio (log10 scale, $10^{-2}-10^2$). The optimization routine aims to minimize:

$$\chi_{1} = (p_{1}(t = \theta_{ss}) - p_{1}(t = \theta_{ind}))^{2}$$
 (28)

$$\chi_2 = (p_2(t = \theta_{ss}) - p_{target})^2 \tag{29}$$

where $\theta_{\rm ind}$ is the time of the induction of p_2 and $\theta_{\rm ss}$ is the last time point, $t_{\rm max}$. If the simulation is not at steady state at $t_{\rm max}$ then the result is given the poorest fitness. $p_{\rm target}$ is calculated by simulating the action of the circuit in a model utilizing the host ribosome pool for gene expression.

Selection of Controller Parameters for Design Guidelines. Coupling and expression scores were calculated for each controller as outlined above for all the results of robustness analysis. These results were then scaled by their maximum absolute values to ensure both axes are between 0 and 1 (note that for calculating the distance metric we can ignore signs):

$$x_{\text{scaled}} = 1 + \frac{\text{coupling}}{\text{max}(\text{lcouplingl})}$$

$$y_{\text{scaled}} = 1 + \frac{\text{expression}}{\text{max}(\text{lexpressionl})}$$
(30)

Given the curved nature of the Pareto front, we recast the Euclidean coordinates into polar coordinates:

$$r = \sqrt{(x_{\text{scaled}}^2 + y_{\text{scaled}}^2)}$$
 $\theta = \arccos(x_{\text{scaled}}/r)$ (31)

We divide the Pareto front into segments ("behaviors") by the corresponding angle θ using the inbuilt MATLAB function discretize. This determines parameter regimes for the given behavior.

ASSOCIATED CONTENT

S Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acssynbio.8b00029.

Supplementary figures and tables; Model reduction; Discussion of parametrization; Circuit models (PDF)

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Notes

The authors declare no competing financial interest.

ACKNOWLEDGMENTS

APSD acknowledges funding from the University of Warwick and the EPRSC & BBSRC Centre for Doctoral Training in Synthetic Biology (grant EP/L01649/1). High performance computational facilities were provided by Warwick Integrative Synthetic Biology Centre, funded by BBSRC/EPSRC (grant BB/M017982/1). JK and JIJ acknowledge support from the European Union's Horizon 2020 research and innovation programme (grant no. 633962) and support from the BBSRC (grant BB/M009769/1).

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